RCA-8462

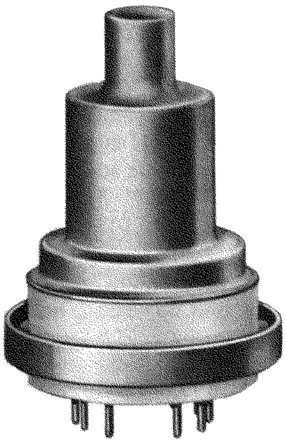
BEAM POWER TUBE

Coaxial-Electrode Structure
Ceramic-Metal Seals
Mesh Filament

Less Than 1-Second Warm-Up
For Use in Low-Voltage Mobile Equipment Up to 500 Mc

2.26" Max. Length
1.44" Max. Diameter
Conduction Cooled

RCA-8462 is a very small, low-cost, conduction-cooled beam power tube designed for use as an rf power amplifier, oscillator, regulator, distributed amplifier, or linear rf power amplifier in mobile or stationary equipment.



Because of its high power sensitivity and high efficiency, the 8462 can be operated with relatively low plate voltage to provide high power output with low driving power. In CW operation with a plate voltage of only 700 volts, the 8462 can provide useful power outputs of 110 watts at 50 Mc, 105 watts at 175 Mc, and 85 watts at 470 Mc.

Less than one-second is required from a cold start to 70% of useful power output. This fast warm-up eliminates stand-by filament power in "push-to-talk" emergency equipment.

The heating time of the mesh filament, however, is a function of filament voltage and the impedance of the filament power supply. To achieve the longest life, the filament voltage should be reduced to the lowest possible value to provide satisfactory operation. Extremely fast "warm-up", less than 100 milliseconds, is also possible by the use of a suitably designed overvoltage control circuit, or "hot-shot" circuit.

The elimination of standby-power and the reduction of operating filament power combine to make the 8462 ideal for mobile equipment.

Featured in the design of the 8462 is its hollow, cylindrical, quick-heating, filamentary cathode comprised of oxide-coated woven wire mesh. This construction provides greater mechanical strength, more emitting surface in a limited space, and lower filament-voltage gradient than conventional filaments.

The 8462 employs a large-area, nickel-plated-copper cylindrical-plate terminal for both high electrical conductivity to the external circuit and high thermal conductivity to the conduction-cooling system.

A low-cost socket may be used to accommodate the 8462. Effective isolation of the output circuit from the input circuit is provided at the higher frequencies by the low-inductance grid-No.2 ring terminal. Grid-No.2 base pins are also available for operation of the 8462 at the lower frequencies.

The three filament-cathode leads provide a low inductance path to rf ground. One of the cathode leads may be series tuned to ground with a capacitor to provide broadband neutralization in the upper frequency range of the tube. The two grid-No.1 leads permit the use of a split-input circuit for distributed amplifier service.

GENERAL DATA

Electrical:

Filamentary Cathode, Woven-Wire-Mesh Type, Oxide-Coated:			
Voltage (AC or DC)	2.9		volts
Current at 2.9 volts	4.6		amp
Minimum heating time	less than 1[a]		sec

See further information on Filament under Electrical Considerations.

Mu-Factor, Grid No.2 to Grid No.1 for plate volts = 250, grid-No.2 volts = 200, and plate amperes = 1.2	11		
Direct Interelectrode Capacitances:[b]			
Grid No.1 to plate	0.13	max.	pf
Grid No.1 to cathode	16		pf
Plate to cathode	0.03	max.	pf
Grid No.1 to grid No.2	22		pf
Grid No.2 to plate	7		pf
Grid No.2 to cathode	3		pf

Mechanical:

Operating Position	Any
Maximum Overall Length	2.26"
Seated Length	1.920" ± 0.065"
Greatest Diameter	1.426" ± 0.010"
Base	Large-Wafer Elevenar 11-Pin with Ring (JEDEC No.E11-81)
Socket	E. F. Johnson Co.† No.124-311-110, Mycalex* No.CP464-2, or equivalent
Grid-No.2 Bypass Capacitor	E. F. Johnson Co.† No.124-113-1, or equivalent
Weight (Approx.)	2 oz

Thermal:

Terminal Temperature (All Terminals)	250	max.	°C
Plate Core Temperature (See *Dimensional Outline*)	250	max.	°C

Cooling, Conduction:
The plate terminal must be thermally coupled to a constant temperature device (heat sink—solid or liquid) to limit the plate terminal temperature to the specified maximum value of 250° C. The grid-No.2, grid-No.1, and filament terminals may also require coupling to the heat sink to limit their respective terminal temperature to the specified maximum value of 250° C.

† E. F. Johnson Co., 1921 10th Ave. S. W., Waseka, Minnesota.

* Mycalex Corp. of America, 725 Clifton Blvd., Clifton, New Jersey.

LINEAR RF POWER AMPLIFIER
Single-Sideband Suppressed-Carrier Service

Peak envelope conditions for a signal having a minimum peak-to-average power ratio of 2

Maximum CCS Ratings, *Absolute-Maximum Values:*

	Up to 500 Mc		
DC PLATE VOLTAGE	2200	max.	volts
DC GRID-No.2 VOLTAGE	400	max.	volts
DC GRID-No.1 VOLTAGE	-100	max.	volts
DC PLATE CURRENT AT PEAK OF ENVELOPE	450[c]	max.	ma
DC GRID-No.1 CURRENT	100	max.	ma
PLATE DISSIPATION	100[d]	max.	watts
GRID No.2 INPUT	8	max.	watts

Typical CCS Operation with "Two-Tone Modulation":

	At 30 Mc	
DC Plate Voltage	700	volts
DC Grid-No.2 Voltage[e]	250	volts
DC Grid-No.1 Voltage[e]	-20	volts
Zero-Signal DC Plate Current	100	ma
Effective RF Load Resistance	1420	ohms
DC Plate Current at Peak of Envelope	205	ma
Average DC Plate Current	150	ma
DC Grid-No.2 Current at Peak of Envelope	16	ma
Average DC Grid-No.2 Current	10	ma
Average DC Grid-No.1 Current	1.0[f]	ma
Peak-Envelope Driver Power Output (Approx.)[g]	0.3	watt
Output-Circuit Efficiency (Approx.)	95	%
Distortion Products Level:[h]		
Third order	30	db
Fifth order	35	db
Useful Power Output (Approx.):		
Average	40[j]	watts
Peak envelope	80[j]	watts

Maximum Circuit Values:

Grid-No.1-Circuit Resistance Under Any Condition:		
With fixed bias	25,000 max.	ohms
With fixed bias (In Class AB_1 operation)	100,000 max.	ohms
With cathode bias	Not recommended	
Grid-No.2 Circuit Impedance	10,000	ohms
Plate Circuit Impedance	See Note k	

RF POWER AMP. & OSCILLATOR — Class C Telegraphy and RF POWER AMPLIFIER — Class C FM Telephony

Maximum CCS Ratings, *Absolute-Maximum Values:*

	Up to 500 Mc		
DC PLATE VOLTAGE	2200	max.	volts
DC GRID-No.2 VOLTAGE	400	max.	volts
DC GRID-No.1 VOLTAGE	-100	max.	volts
DC PLATE CURRENT	300	max.	ma
DC GRID-No.1 CURRENT	100	max.	ma
GRID-No.2 INPUT	8	max.	watts
PLATE DISSIPATION	100[d]	max.	watts

Typical CCS Operation:

In Grid-Drive Circuit at 50 Mc

DC Plate Voltage	500	700	volts
DC Grid-No.2 Voltage	160	175	volts
DC Grid-No.1 Voltage	-10	-10	volts
DC Plate Current	300	300	ma
DC Grid-No.2 Current	25	25	ma
DC Grid-No.1 Current	50	50	ma
Driver Power Output (Approx.)[m]	1.2	1.2	watts
Useful Power Output	85[j]	110[j]	watts

In Grid-Drive Circuit at 175 Mc

DC Plate Voltage	500	700	volts
DC Grid-No.2 Voltage	200	200	volts
DC Grid-No.1 Voltage	-30	-30	volts
DC Plate Current	300	300	ma
DC Grid-No.2 Current	30	20	ma
DC Grid-No.1 Current	40	40	ma
Driver Power Output (Approx.)[m]	3	3	watts
Useful Power Output	70[j]	105[j]	watts

In Grid-Drive Circuit at 470 Mc

DC Plate Voltage	700	volts
DC Grid-No.2 Voltage	200	volts
DC Grid-No.1 Voltage	-30	volts
DC Plate Current	300	ma
DC Grid-No.2 Current	10	ma
DC Grid-No.1 Current	20	ma
Driver Power Output (Approx.)[m]	5	watts
Useful Power Output	85[j]	watts

Maximum Circuit Values:

Grid-No.1-Circuit Resistance Under Any Condition:		
With fixed bias	25,000 max.	ohms
Grid-No.2 Circuit Impedance	10,000 max.	ohms
Plate Circuit Impedance	See Note k	

CHARACTERISTICS RANGE VALUES

	Note	*Min.*	*Max.*	
1. Filament Current	1	3.6	5.6	amp
2. Direct Interelectrode Capacitances:				
Grid No.1 to plate	2	-	0.13	pf
Grid No.1 to cathode	2	14	18.5	pf
Plate to cathode	2	-	0.03	pf
Grid No.1 to grid No.2	2	18	24	pf
Grid No.2 to plate	2	5.7	8.0	pf
Grid No.2 to cathode	2	2.0	4.0	pf
3. Grid-No.1 Voltage	1,3	-6	-24	volts
4. Grid-No.2 Current	1,3	-7	+8	ma

Note 1: With 2.9 volts (AC or DC) on filament.

Note 2: Measured with special shield adapter.

Note 3: With dc plate voltage of 700 volts, dc grid-No.2 voltage of 250 volts, and dc grid-No.1 voltage adjusted to give a dc plate current of 185 ma.

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[a] The heating time required for adequate cathode emission is a function of the filament voltage and the impedance of the filament-voltage supply. It may be drastically reduced by employing a suitably designed overvoltage control circuit.

[b] Measured with special shield adapter.

[c] The maximum rating for a signal having a minimum peak-to-average power ratio less than 2, such as is obtained in "Single-Tone" operation, is 300 ma. During short periods of circuit adjustment under "Single-Tone" conditions, the average plate current may be as high as 450 ma.

[d] Maximum plate dissipation is limited by the maximum plate core temperature and the cooling system to maintain tube operation below the specified maximum plate core temperature. With simple low-cost cooling techniques, maximum plate dissipation may be only about 100 watts; with more sophisticated cooling techniques, maximum plate dissipation may be as high as 300 watts.

[e] Obtained preferably from a separate well-regulated source.

[f] This value represents the approximate grid-No.1 current obtained due to initial electron velocities and contact-potential effects when grid No.1 is driven to zero volts at maximum signal.

[g] Driver power output represents circuit losses and is the actual power measured at input to grid-No.1 circuit. The actual power required depends on the operating frequency and the circuit used. The tube driving power is approximately zero watts.

[h] With maximum signal output used as a reference, and without the use of feedback to enhance linearity.

[j] This value of useful power is measured at load of output circuit.

[k] The tube should see an effective plate supply impedance which limits the peak current through the tube under surge conditions to 15 amperes.

[m] Driver power output includes circuit losses and is the actual power measured at the input to the grid circuit. It will vary depending upon the frequency of operation and the circuit used.

DEFINITIONS

CCS — Continuous Commercial Service.

Rating System — The *maximum ratings* in the tabulated data are established in accordance with the following definition of the *Absolute-Maximum Rating System* for rating electron devices.

Absolute-Maximum ratings are limiting values of operating and environmental conditions applicable to any electron device of a specified type as defined by its published data, and should not be exceeded under the worst probable conditions.

The device manufacturer chooses these values to provide acceptable serviceability of the device, taking no responsibility for equipment variations, environment variations, and the effects of changes in operating conditions due to variations in device characteristics.

The equipment manufacturer should design so that initially and throughout life no absolute-maximum value for the intended service is exceeded with any device under the worst probable operating conditions with respect to supply-voltage variation, equipment component variation, equipment control adjustment, load variation, signal variation, environmental conditions, and variations in device characteristics.

Two-Tone Modulation — Two-Tone Modulation operation refers to that class of amplifier service in which the input consists of two monofrequency rf signals having equal peak amplitude.

GENERAL CONSIDERATIONS

Temperature

The maximum terminal temperature of 250° C and the maximum plate core temperature of 250° C are tube ratings and are to be observed in the same manner as other ratings. The temperature may be measured with temperature-sensitive paint, such as Tempilaq. The latter is made by the Tempil Corporation, 132 W.22nd Street, New York 11, N.Y.

Mounting

The 8462 may be mounted by a variety of techniques; however, the frequency of operation and the heat sink to be used will narrow the selection. The base socket, finger-stock grid-No.2 ring (if used), or plate-conduction clamp used in the tube mounting may be fixed. The remaining connector (s) must be adjustable in a plane normal to the major tube axis to compensate for variations in concentricity for the associated parts of the tube.

STRUCTURAL ARRANGEMENT

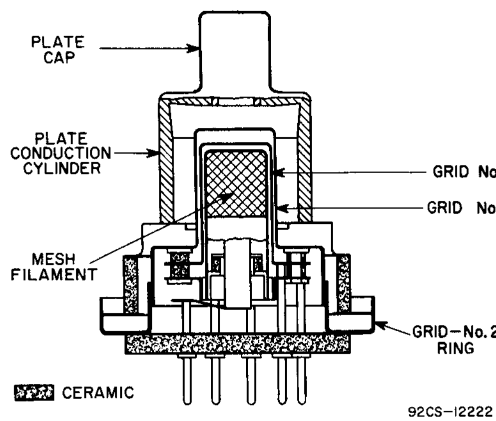


Fig.1

The plate cap is primarily a protective covering for the exhaust tip-off but may be used as the plate terminal by using a flexible cap connector; it may not be clamped, nor form a portion of the cooling system.

ELECTRICAL CONSIDERATIONS

Filament

The filament of the 8462 should be operated at constant voltage rather than constant current. Voltages to other electrodes may be applied simultaneously with the rated filament voltage.

The life of the cathode can be conserved by operating at the lowest filament supply voltage which will give the desired performance. Good regulation of the filament supply voltage is, in general, economically advantageous from the viewpoint of tube life; for constant voltage operation, the voltage fluctuations should not be more than 5%. This recommendation is particularly applicable at the higher operating frequencies.

Grid No. 1

Grid No.1 of the 8462 in uhf service is subjected to heating caused not only by the normal electron bombardment as indicated by the grid current, but also by radiation from the cathode and circulating rf currents. For these reasons, more than ordinary care must be taken during operation to prevent exceeding the grid-No.1 current rating and the maximum grid-No.1 terminal temperature rating.

TYPICAL PLATE CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 400 Volts

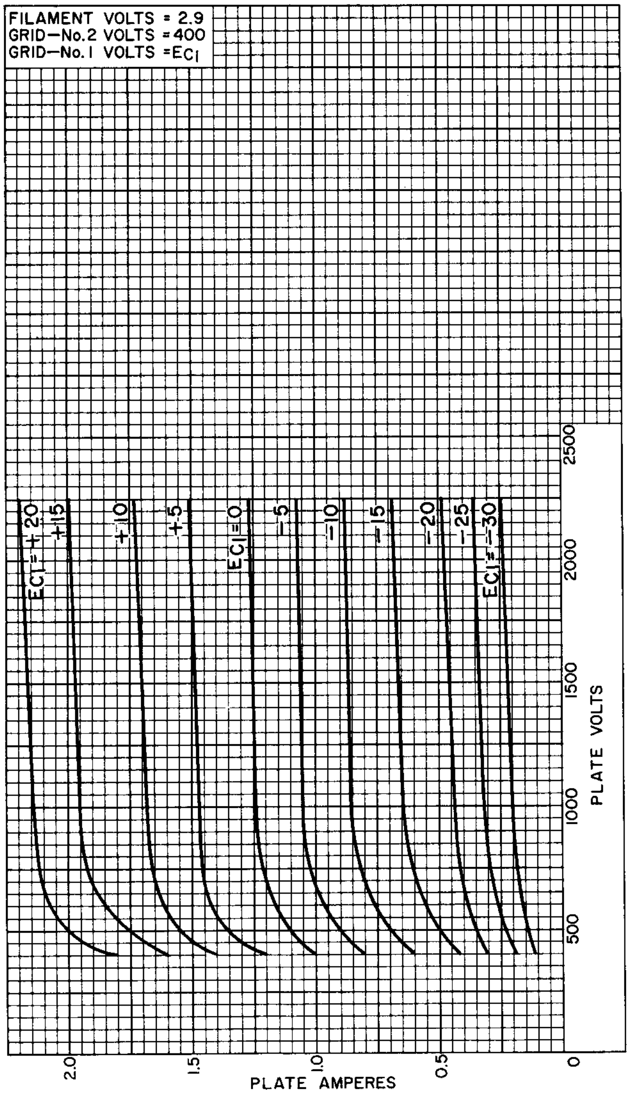


Fig.2

Grid No. 2

The grid-No.2 current of the 8462 may be negative under certain operating conditions. The voltage for grid No.2 should be obtained from a source of good regulation; if a separate source is used, a maximum impedance of 10,000 ohms and a minimum divider current of 40 milliamperes are required; if a voltage divider from the plate supply is used, a maximum impedance of 10,000 ohms between the grid-No.2 and ground is required. The plate voltage should be applied before or simultaneously with grid-No.2 voltage; otherwise, with voltage on grid-No.2 only, its current may be large enough to cause excessive grid-No.2 dissipation.

TYPICAL CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 400 Volts

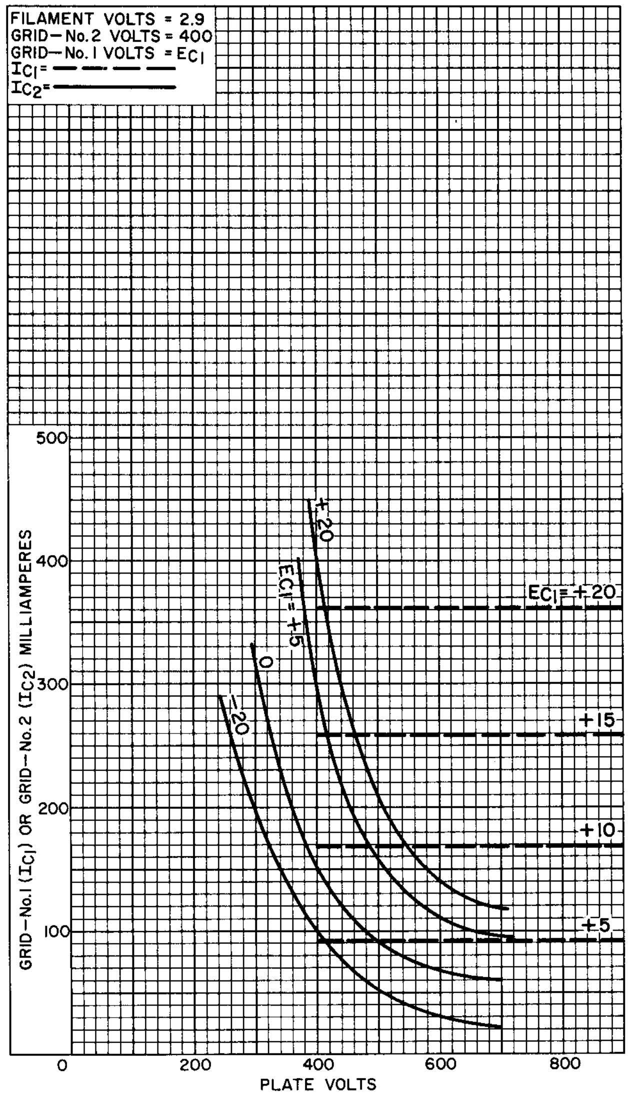
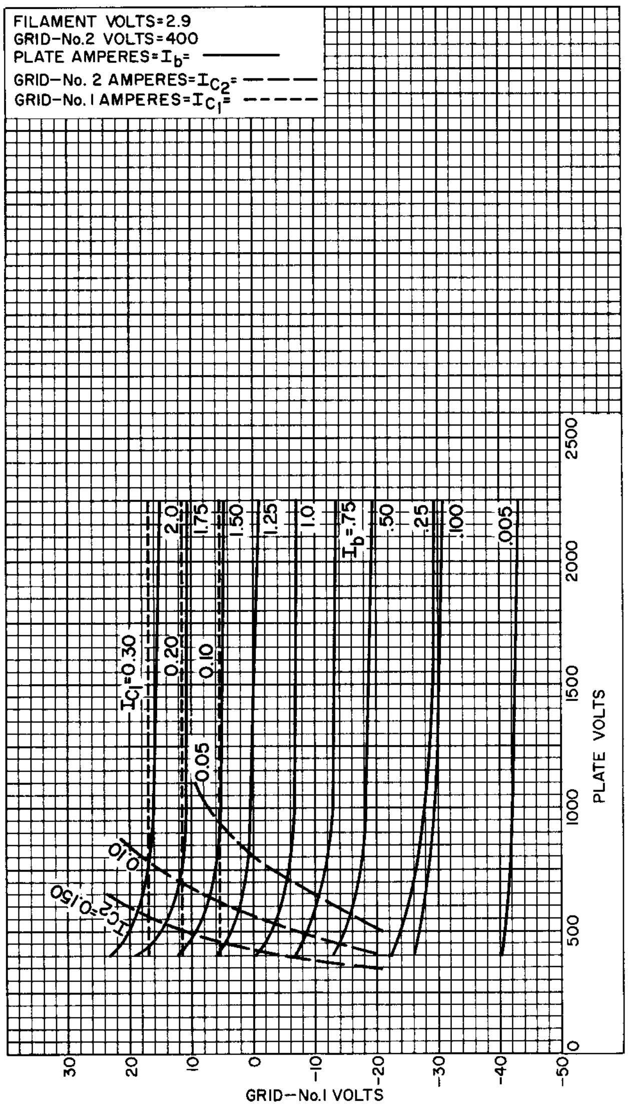


Fig.3

The grid-No.2 current is a very sensitive indication of plate-circuit loading. When the 8462 is operated without load, the grid-No.2 current rises excessively, often to a value which damages the tube. Therefore, care should be taken when tuning the 8462 circuit under no-load or lightly loaded conditions to prevent exceeding the grid-No.2 input rating of the tube. In this connection, reduction of the grid-No.2 voltage will be helpful.

tubes due to internal flashing is more prevalent when the circuit is not tuned to optimum conditions. Even though laboratory tests indicate that no such protection is needed, poor circuit adjustment in the field may result in shortened tube life.

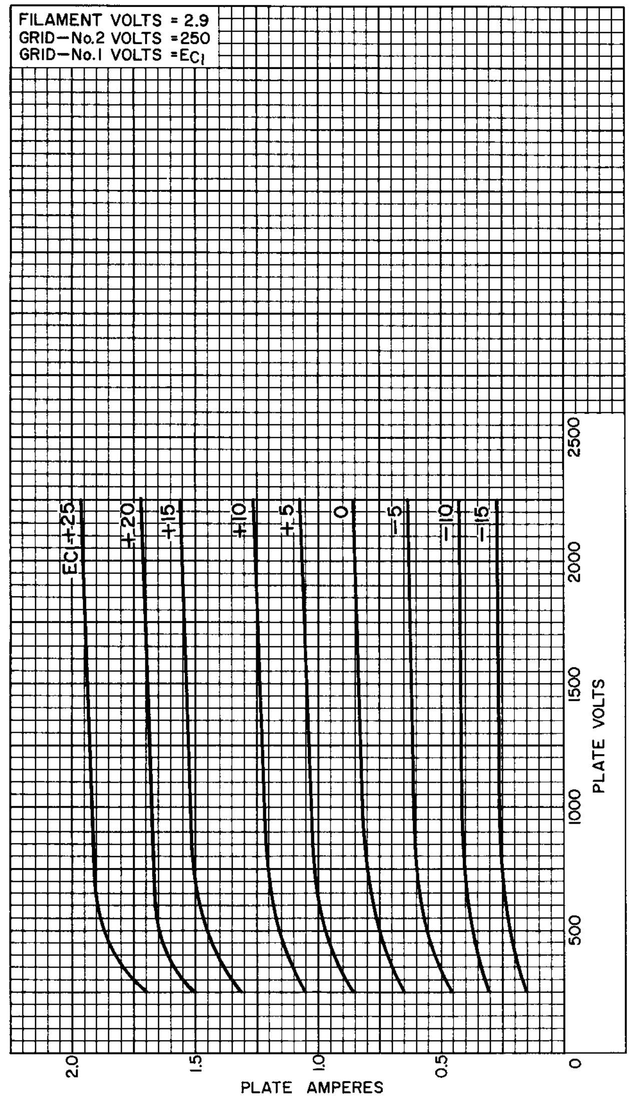
TYPICAL CONSTANT-CURRENT CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 400 Volts



92CM-12227

Fig.4

TYPICAL PLATE CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 250 Volts



92CM-12228

Fig.5

Plate

In tubes, such as the 8462, having very closely spaced electrodes, extremely high voltage gradients occur even with moderate tube operating voltages. Any tube flash-arcing may be destructive. It is recommended that each tube see an effective plate supply impedance which limits the peak current through the tube under surge conditions to 15 amperes. Failure of the

Driver

The driver power output shown in the typical operation of the 8462 in rf service is considerably more than is normally calculated for typical driving power input in order to permit considerable range of adjustment, and also to provide for losses in the grid-No.1 circuits and the coupling circuits. This consideration is particularly important at the higher frequencies where circuit losses, radiation losses, and transit-time losses increase, and the effects of cathode-lead inductive reactance becomes significant.

Class C RF Telegraphy Service

In class C rf telegraphy service, the 8462 may be supplied with bias by any convenient method

TYPICAL CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 250 Volts

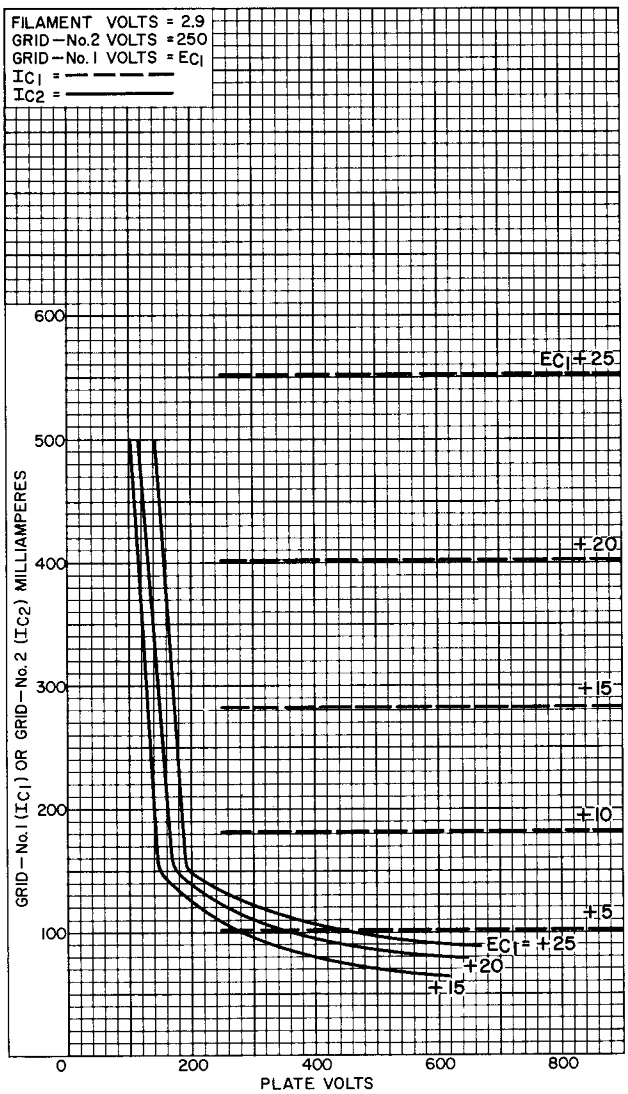


Fig.6

except when the tube is used in the final amplifier or a preceding stage of a transmitter designed for break-in operation and oscillator keying. In this case, an amount of fixed bias must be used to limit the plate current and, therefore, the plate dissipation to a safe value.

Protective Devices

Protective devices should be used to protect not only the plate but also grid No.2 against overload. In order to prevent excessive plate-current flow and resultant overheating of the tube, the common ground lead of the plate circuit should be connected in series with the coil of an instantaneous overload relay. This relay should be adjusted to remove the dc plate and grid-No.2 voltage when the average value of plate current

TYPICAL CONSTANT-CURRENT CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 250 Volts

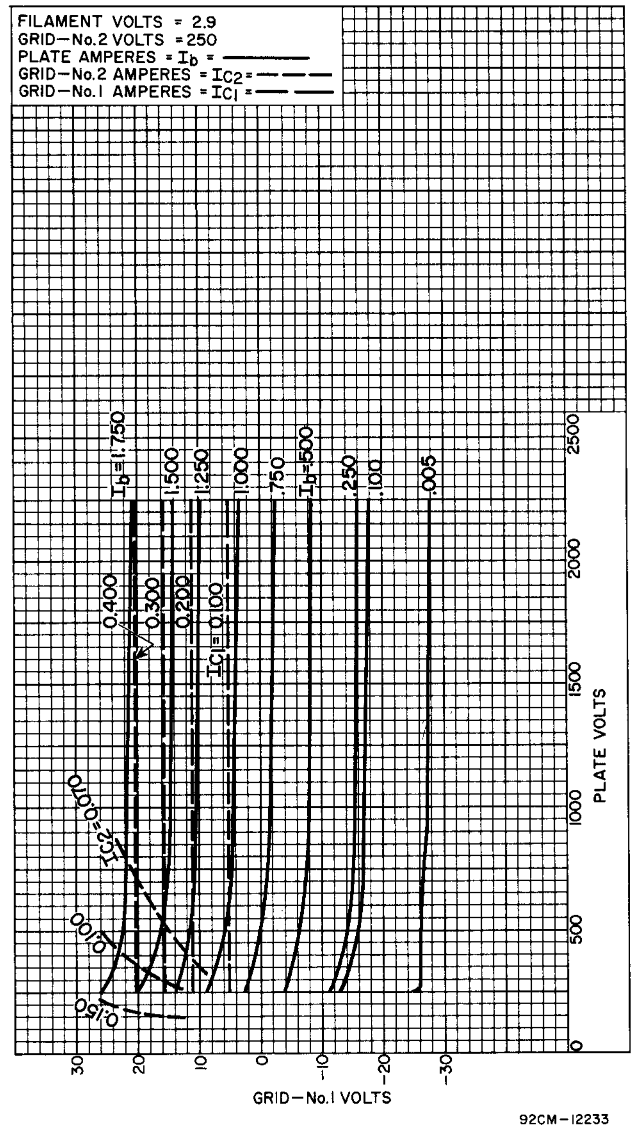


Fig.7

reaches a value slightly higher than normal plate current. A protective device in the grid-No.2 supply should remove the grid-No.2 voltage when the dc grid-No.2 current reaches a value slightly higher than normal.

Precautions

The rated plate and grid-No.2 voltages of this tube are extremely dangerous. Great care should be taken during the adjustment of circuits.

The tube and its associated apparatus, especially all parts which may be at high potential above ground, should be housed in a protective enclosure. The protective housing should be designed with interlocks so that personnel can not possibly come in contact with any high-potential point in the electrical system. The interlock devices should function to break the primary circuit of the high-voltage supplies when any gate or door on the protective housing is opened, and should prevent the closing of the primary circuit until the door is again locked.

TYPICAL PLATE CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 150 Volts

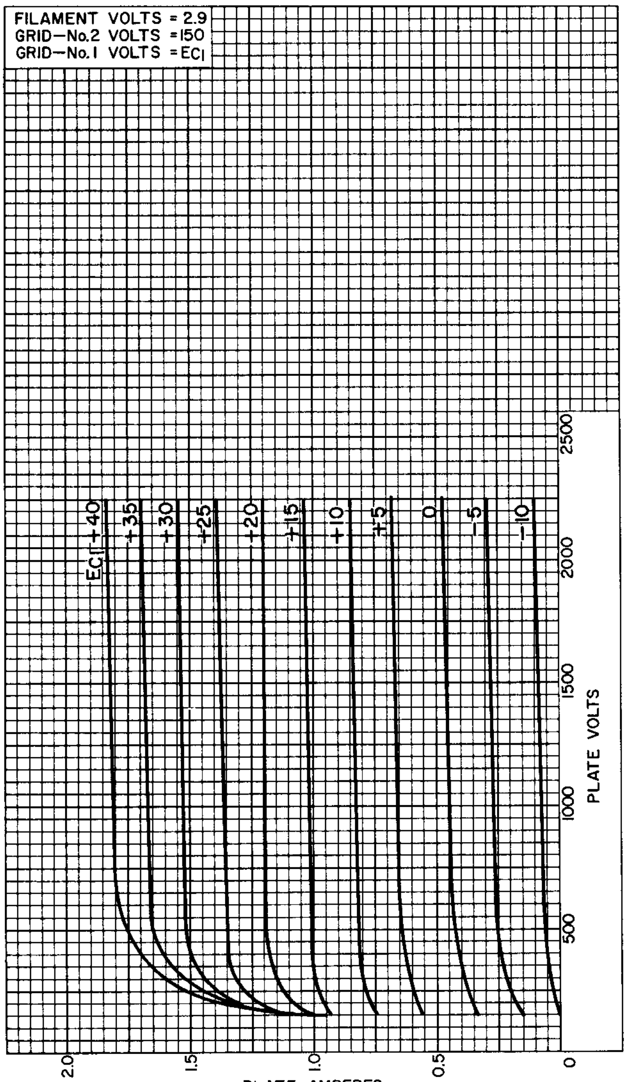


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Fig.8

COOLING CONSIDERATIONS

System

The conduction-cooling system consists, in general, of a constant temperature device (heat sink) and suitable heat-flow path (coupling) between the heat sink and tube. Primary consideration of the system should be given to the design of a heat-flow path (coupling device) with high thermal conductivity.

Thermal conductivity is defined as the time rate of transfer of heat by conduction, through unit thickness, across unit area for unit difference of temperature. It is measured in watts per square inch for a thickness of one inch and a difference of temperature of 1° C (See *Table of Conversion Factors for Thermal Conductivity)* as shown in the following equation:

$$K = \frac{W}{A\frac{(T_2 - T_1)}{L}} \qquad (1)$$

TYPICAL CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 150 Volts

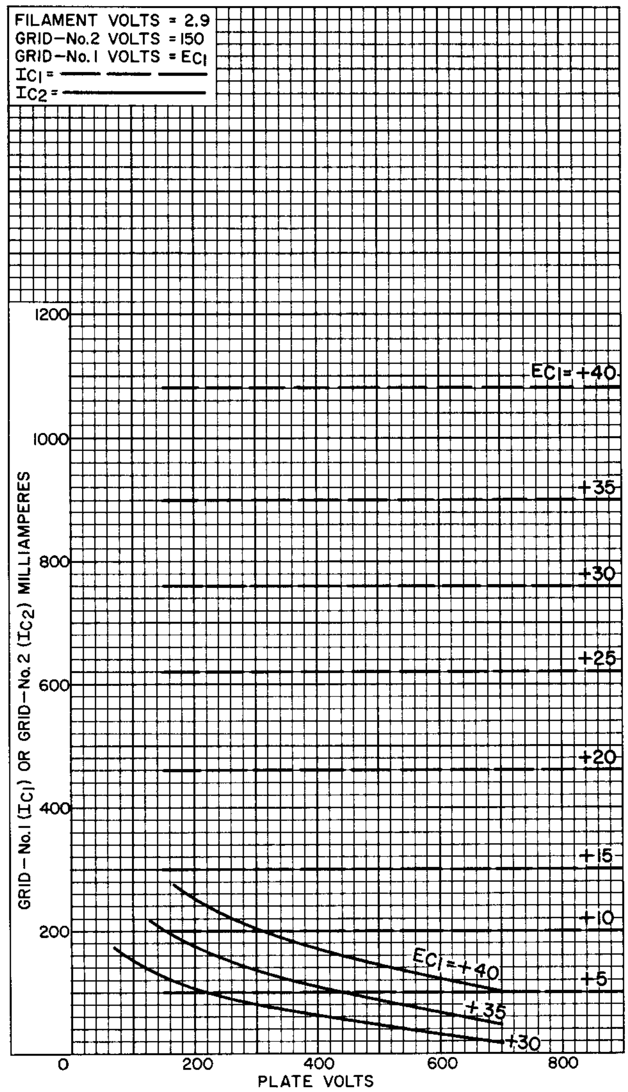

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Fig.9

where;

K = thermal conductivity of the material

W = power transfer in watts

A = area measured at right angles to the direction of the flow of heat in square inches

T_1, T_2 = temperature in degrees Centigrade of planes or surfaces under consideration

L = length of heat path in inches through coupling material to produce temperature gradient

For a given system Equation (1) must be integrated to consider changes in area (A) dependent on the coupling configuration and changes in thermal conductivity (K) dependent on various coupling materials and interfaces. Equation (1) may now be reduced to the following:

$$K_s = \frac{W_p}{T_2 - T_1} \qquad (2)$$

where;

K_s = thermal conductance of the system

W_p = maximum permissible plate dissipation in watts

T_2 = temperature in degrees Centigrade at tube terminal

Note: *This value may never exceed the specified maximum rating for terminal temperature.*

T_1 = temperature in degrees Centigrade of heat sink

Heat Sink

The heat sink should be designed to act as a constant-temperature device; that is, to prevent any increase in temperature by dissipating the heat beyond the equipment compartment. Heat sinks can take the form of solids or liquids. In most applications such a heat sink is available in the form of equipment chassis, plate line, or output cavity. Mechanically, the equipment chassis is the most practical heat sink as shown in Reference 1. At uhf frequencies, coaxial elements, tuned lines or cavities become more feasible because of increasing rf losses across supports to equipment chassis.

Coupling

There are numerous insulating materials available to serve as the heat-coupling device such as beryllium oxide (beryllia), high-aluminum oxide (high alumina), mica and other insulating bodies. The thermal conductivity of these insulators varies considerably. The choice of insulator will then be dependent primarily on the plate dissipation in the given application. As shown in Fig. 11 beryllia has much higher thermal conductivity than its nearest competitor, high alumina.

Beryllia provides the unique properties required for coupling the tube to the heat sink: low electric conductivity (volume resistivity-

TYPICAL CONSTANT-CURRENT CHARACTERISTICS
At a Constant Grid-No.2 Voltage of 150 Volts

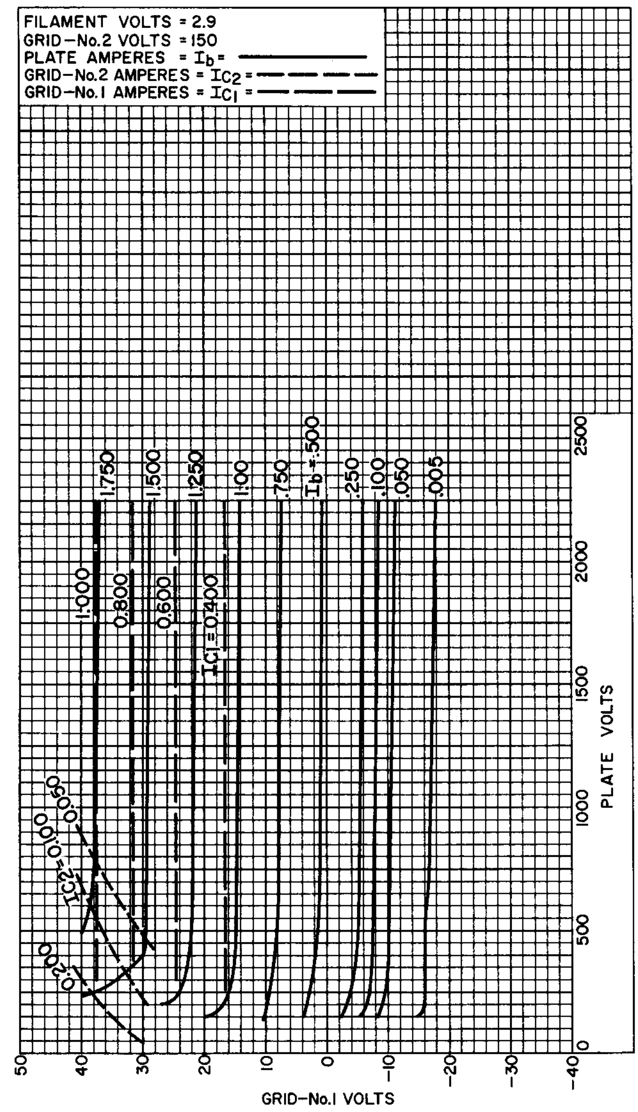


Fig.10

10^{16} ohm-cm) and high thermal conductivity (2.9 watts/in^2 - $^{\circ}$C at 200° C).

Precaution: Beryllia dust and fumes are highly toxic to mucous membranes and may cause serious ulcers when imbedded under the skin. See References 2, 3, and 4.

At low frequencies the inductive element of the plate circuit is usually a relatively long coil which does not provide a good thermal path from plate to chassis. The shunt capacity is large, however, and heat can be conducted through a portion of it to the chassis. At high frequencies the shunt capacity of the plate circuit is limited but the inductive element is short and can be made with sufficient cross-sectional area to form an excellent thermal path.

Conduction Properties of the Tube

The cylindrical plate terminal is nickel-plated copper with high thermal conductivity to conduct the heat of plate dissipation to the surface of the plate terminal. The cooling system for a given application should be designed to dissipate the heat from the tube. The matching coupler to the tube should have a surface to provide intimate thermal contact with the plate terminal. See Reference 7.

It may also be necessary to couple grid No.2, grid No.1, filament-cathode, and filament terminals to the heat sink. In all cases it is necessary to maintain all terminals at a temperature under the maximum temperature of 250° C. Tube life can be increased by maintaining all terminal temperatures substantially below the maximum temperature rating.

HEAT-TRANSFER CHARACTERISTICS
of Various Materials

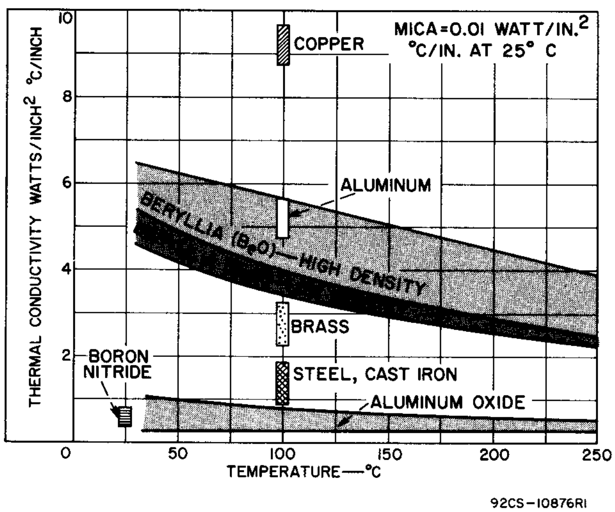


Fig.11

TABLE OF CONVERSION FACTORS FOR THERMAL CONDUCTIVITY

Multiply	by	To Get
B.T.U./(sq ft)(hr)(°F/ft)	.0440	watts/(sq in)(°C/in)
B.T.U./(sq ft)(hr)'°F/in)	.00367	watts/(sq in)(°C/in)
calories/(sq cm)(sec)(°C/cm)	10.66	watts/(sq in)(°C/in)
watts/(sq cm)(°C/cm)	2.54	watts/(sq in)(°C/in)

REFERENCES

1. J.E. Brosz and R.H. Decker, *"Beryllia Aids Equipment Cooling"*, Electronic Equipment Engineering, Jan. 1960.
2. D.W. White, Jr., and J.E. Burke, *"The Metal Beryllium"* (book), published by the American Society for Metals, Cleveland, Ohio.
3. Donald P. O'Neil, *"Toxic Materials Machined Safely"*, American Machinist, June 4, 1955.
4. Sidney Laskin, Robert A.N. Turner, and Herbert E. Stokinger, *"Analysis of Dust and Fume Hazards in a Beryllium Plant"*, U.S. Atomic Energy Commission, MDDC-1355.
5. James J. Gangler, *"Some Physical Properties of Eight Refractory Oxides and Carbides"*, American Ceramic Society Journal, Vol. 33, December 1950.
6. W.D. Kingery, J. Francl, R.L. Coble, and T. Vasilos, *"Thermal Conductivity X — Data for Several Pure Oxide Materials Corrected to Zero Porosity"*, American Ceramic Society Journal, Vol. 37, February 1954.
7. Graff, *"Thermal Conductance Across Metal Joints"*, Machine Design, September 15, 1960.
8. John W. Gaylord, *"Conduction Cooling of Power Tubes in Vehicular Communication Equipment"*, IEEE PTGVC Transactions, Vol. 12, September 1963.

BERYLLIA PRODUCTS MAY BE OBTAINED FROM THE FOLLOWING REPRESENTATIVE LIST OF SUPPLIERS:

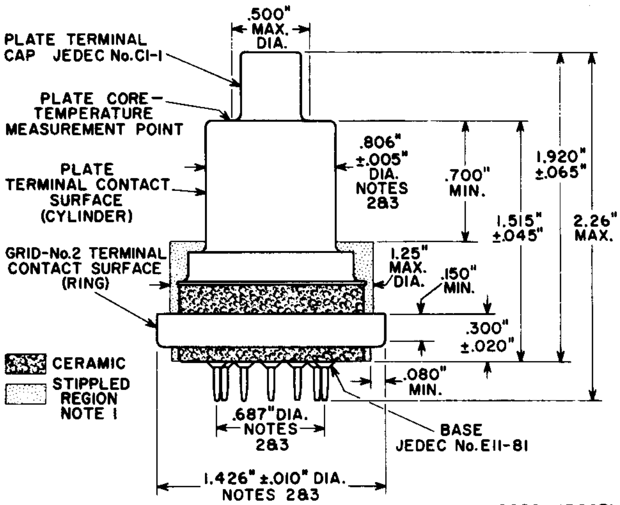
National Beryllia Corp.
First & Haskell Aves.
Haskell, N.J.

Brush Beryllium Corp.
5209 Euclid Ave.
Cleveland 3, Ohio

The Beryllium Corp. of America
P.O. Box 1462
Reading, Pennsylvania

Frenchtown Porcelain Co.
Eighth & Harrison Sts.
Frenchtown, New Jersey

DIMENSIONAL OUTLINE



NOTE 1: KEEP ALL STIPPLED REGIONS CLEAR. DO NOT ALLOW CONTACTS OR CIRCUIT COMPONENTS TO PROTRUDE INTO THESE ANNULAR VOLUMES.

NOTE 2: THE DIAMETERS OF THE PLATE TERMINAL CONTACT SURFACE, GRID-No.2 TERMINAL CONTACT SURFACE, AND PIN CIRCLE TO BE CONCENTRIC WITHIN THE FOLLOWING VALUES OF MAXIMUM FULL INDICATOR READING:

Plate Terminal Contact Surface to Grid-No.2 Terminal Contact Surface. . . 0.030"

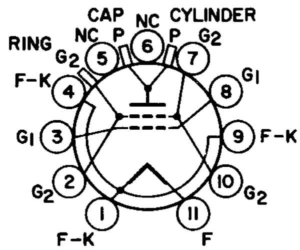
Plate Terminal Contact Surface to Pin Circle. . . . . 0.040"

Grid-No.2 Terminal Contact Surface to Pin Circle. . . . . 0.030"

NOTE 3: THE FULL INDICATOR READING IS THE MAXIMUM DEVIATION IN RADIAL POSITION OF A SURFACE WHEN THE TUBE IS COMPLETELY ROTATED ABOUT THE CENTER OF THE REFERENCE SURFACE. IT IS A MEASURE OF THE TOTAL EFFECT OF RUN-OUT AND ELLIPTICITY.

TERMINAL CONNECTIONS

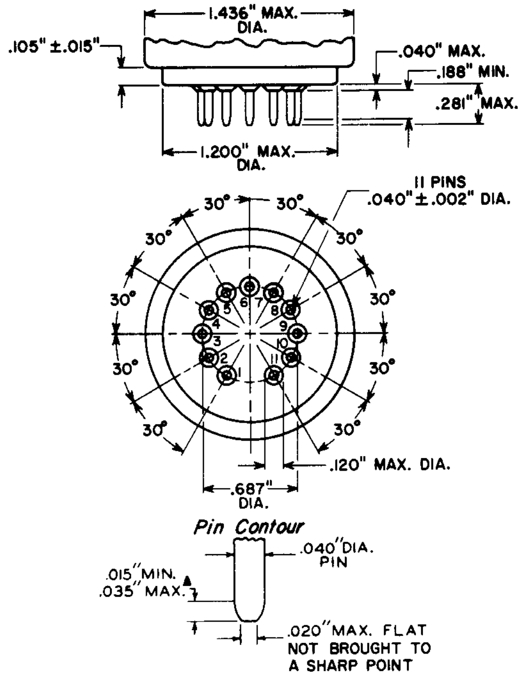
PIN 1: FILAMENT-CATHODE
PIN 2: GRID No.2
PIN 3: GRID No.1
PIN 4: FILAMENT-CATHODE
PIN 5: NO CONNECTION
PIN 6: NO CONNECTION
PIN 7: GRID No.2
PIN 8: GRID No.1
PIN 9: FILAMENT-CATHODE



PIN 10: GRID No.2
PIN 11: FILAMENT
CAP: PLATE TERMINAL CONNECTION
CYLINDER: PLATE TERMINAL CONTACT SURFACE (To contact to conduction-cooling system)
RING: GRID-No.2 TERMINAL CONTACT SURFACE (For use at higher frequencies)

BASE DRAWING

LARGE-WAFER ELEVENAR 11-PIN WITH RING JEDEC No.E11-81



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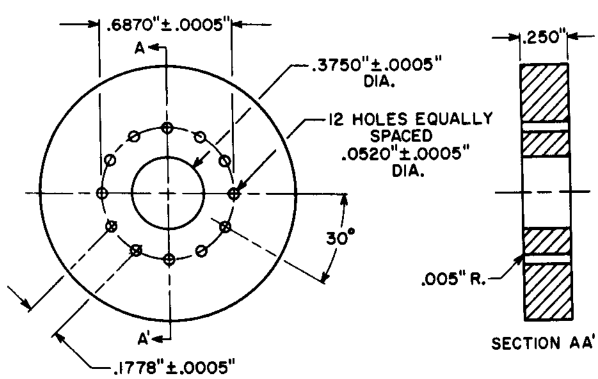
* THIS DIMENSION AROUND THE PERIPHERY OF ANY INDIVIDUAL PIN MAY VARY WITHIN THE LIMITS SHOWN.

GAUGE DRAWING

JEDEC No.GE11-1



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