

# UCH 41

## UCH 41 Triode-hexode frequency changer

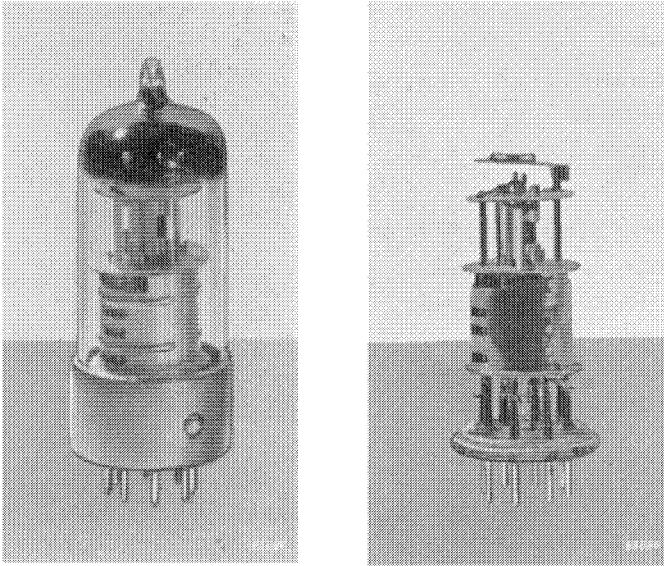


Fig. 1  
The UCH 41, showing the electrode system (approximately actual size).

The triode-hexode UCH 41 is a frequency changer with a conversion conductance of  $450 \mu\text{A/V}$  at an applied voltage of  $170 \text{ V}$ , or  $320 \mu\text{A/V}$  at  $100 \text{ V}$ . Further particulars will be found in the description of the ECH 41, the corresponding E-type valve.

### TECHNICAL DATA OF THE TRIODE-HEXODE UCH 41

#### Heater data

Heating : indirect, A.C. or D.C., series feed

Heater current . . . . . $I_f$	=	100 mA
Heater voltage . . . . . $V_f$	=	14 V

#### Capacitances (cold valve)

##### Hexode section

Input capacitance . . . . . $C_{g1}$	=	3.4 pF
Output capacitance . . . . . $C_a$	=	6.0 pF
Anode - control grid . . . . . $C_{ag1}$	<	0.1 pF
Heater - control grid . . . . . $C_{o1f}$	<	0.15 pF

Triode section

Input capacitance . . . . .	$C_{gT+g3}$	=	4.9 pF
Output capacitance . . . . .	$C_a$	=	1.5 pF
Anode - grid . . . . .	$C'(gT+g3)_a$	=	1.2 pF

Between triode and hexode sections

Hexode control grid - triode grid	$C_{g1H-(gT+g3)}$	<	0.35 pF
Hexode anode - triode grid . .	$C_{aH-(gT+g3)}$	<	0.2 pF

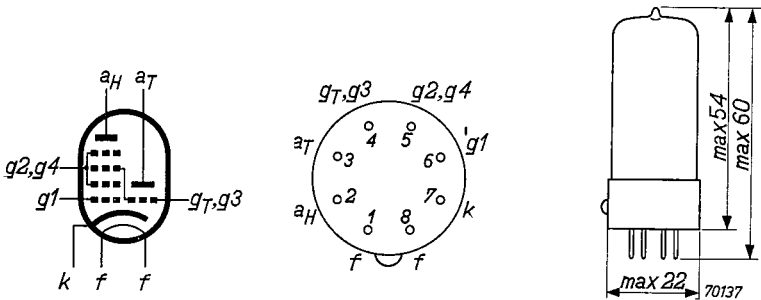


Fig. 2

Electrode arrangement, electrode connections and maximum dimensions in mm of the UCH 41.

Operating characteristics of the hexode section used as frequency changer (screen grids fed by means of a potentiometer ; see Figs. 6—13 incl.)

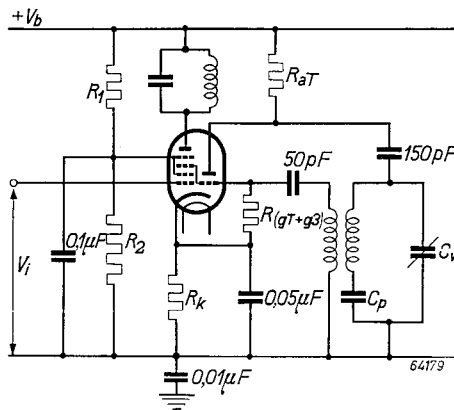


Fig. 3

# UCH 41

Anode and supply voltage . . . . .	$V_a = V_b$	=	100	170	V		
Resistor between supply voltage and screen grids . . . . .	$R_1$	=	22	22	k $\Omega$		
Resistor between screen grids and chassis . . . . .	$R_2$	=	47	47	k $\Omega$		
Bias resistor . . . . .	$R_k$	=	200	200	$\Omega$		
Oscillator grid leak . . . . .	$R_{gT+g3}$	=	20	20	k $\Omega$		
Oscillator grid current . . . . .	$I_{gT+g3}$	=	200	320	$\mu$ A		
Grid bias . . . . .	$V_{g1}$	=	$\overbrace{-1.0 \quad -14}$	$\overbrace{-1.8 \quad -22}$	V		
Screen grid voltage . . . . .	$V_{g2+g4}$	=	52	68	87	116	V
Anode current . . . . .	$I_a$	=	1.0	—	2.2	—	mA
Screen grid current . . . . .	$I_{g2+g4}$	=	1.0	—	1.9	—	mA
Conversion conductance . . . . .	$S_c$	=	320	3.2	450	4.5	$\mu$ A/V
Internal resistance . . . . .	$R_i$	=	1.4	>5	1.2	>5	M $\Omega$
Equivalent noise resistance . . . . .	$R_{eq}$	=	115	—	145	—	k $\Omega$

Anode and supply voltage . . . . .	$V_a = V_b$	=	200	V	
Resistor between supply voltage and screen grids . . . . .	$R_1$	=	22	k $\Omega$	
Resistor between screen grids and chassis . . . . .	$R_2$	=	47	k $\Omega$	
Bias resistor . . . . .	$R_k$	=	225	$\Omega$	
Oscillator grid leak . . . . .	$R_{gT+g3}$	=	20	k $\Omega$	
Oscillator grid current . . . . .	$I_{gT+g3}$	=	360	$\mu$ A	
Grid bias . . . . .	$V_{g1}$	=	$\overbrace{-2.2 \quad -27}$	V	
Screen grid voltage . . . . .	$V_{g2+g4}$	=	105	136	V
Anode current . . . . .	$I_a$	=	3.0	—	mA
Screen grid current . . . . .	$I_{g2+g4}$	=	2.1	—	mA
Conversion conductance . . . . .	$S_c$	=	500	5	$\mu$ A/V
Internal resistance . . . . .	$R_i$	=	1.0	>5	M $\Omega$
Equivalent noise resistance . . . . .	$R_{eq}$	=	220	—	k $\Omega$

## Typical characteristics of the triode section (see Figs. 15 and 16)

Anode voltage . . . . .	$V_a$	=	100	V
Grid voltage . . . . .	$V_{gT+g3}$	=	0	V
Anode current . . . . .	$I_a$	=	8.5	mA
Mutual conductance . . . . .	$S$	=	1.9	mA/V
Amplification factor . . . . .	$\mu$	=	19	

## Operating characteristics of the triode section used as oscillator

(see Figs. 17 and 18)

Supply voltage . . . . .	$V_b$	=	100	170	200	V
Anode resistor . . . . .	$R_a$	=	10	10	20	k $\Omega$
Anode current . . . . .	$I_a$	=	2.8	4.9	4.6	mA
Oscillator grid leak . . . . .	$R_{gT+g3}$	=	20	20	20	k $\Omega$
Oscillator grid current . . . . .	$I_{gT+g3}$	=	200	320	360	$\mu$ A
Oscillator voltage . . . . .	$V_{osc}$	=	4	7	8	V <sub>RMS</sub>
Effective slope . . . . .	$S_{eff}$	=	0.56	0.6	0.5	mA/V

Operating characteristics of the UCH 41 used as phase inverter (see Fig. 4)

Supply voltage	Total current	Amplification	Distortion (%) at an output voltage of	
			5 V <sub>RMS</sub>	10 V <sub>RMS</sub>
100	1.2	10	1.5	—
170	2.0	10	1.0	1.8

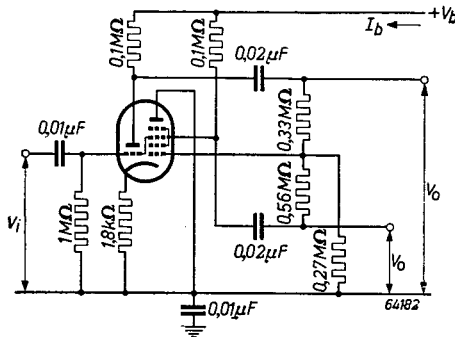


Fig. 4  
The UCH 41 used as phase inverter.

Operating characteristics of the hexode section used as frequency changer with screen grids, fed, together with that of the UAF 42, by means of a common potentiometer (see Figs. 19—21)

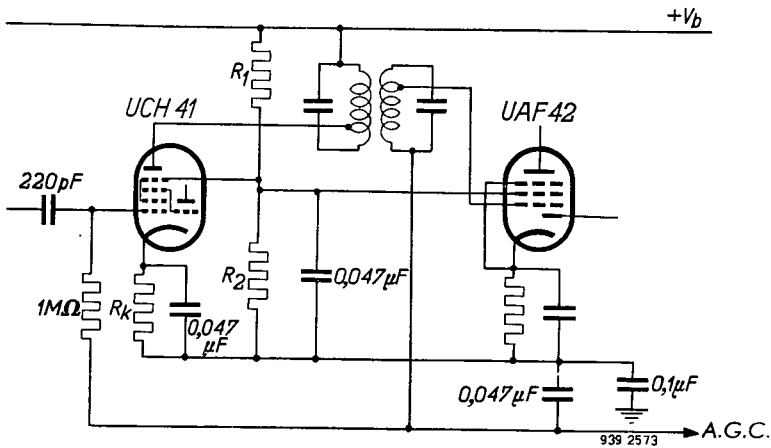


Fig. 5

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## UCH 41

Anode and supply voltage . . .	$V_a = V_b =$	100	170	V	
Resistor between supply voltage and screen grids . . . . .	$R_1 =$	12	12	k $\Omega$	
Resistor between screen grids and chassis . . . . .	$R_2 =$	27	27	k $\Omega$	
Bias resistor . . . . .	$R_k =$	200	200	$\Omega$	
Oscillator grid leak . . . . .	$R_{gT+g3} =$	20	20	k $\Omega$	
Oscillator grid current . . . . .	$I_{gT+g3} =$	200	320	$\mu$ A	
Grid bias . . . . .	$V_{g1} =$	-1.0 -10.5 -1.8 -18 V			
Screen grid voltage . . . . .	$V_{g2+g4} =$	53	69	87	117 V
Anode current . . . . .	$I_a =$	1.0	—	2.2	— mA
Screen grid current . . . . .	$I_{g2+g4} =$	1.0	—	1.9	— mA
Conversion conductance . . . . .	$S_c =$	320	10	450	11 $\mu$ A/V
Internal resistance . . . . .	$R_i =$	1.4	—	1.2	— M $\Omega$
Equivalent noise resistance . . . . .	$R_{eq} =$	115	—	145	— k $\Omega$

**Operating characteristics of the hexode section of the UCH 41 used as frequency changer;** screen grid voltage, together with that of the I.F. amplifier UF 41 derived from a common potentiometer (circuit corresponding to that shown in Fig. 5)

Anode and supply voltage . . .	$V_a = V_b =$	100	170	V	
Potentiometer for screen grid feed . . . . .	$R_1 =$	12	12	k $\Omega$	
	$R_2 =$	27	27	k $\Omega$	
Bias resistor . . . . .	$R_k =$	200	200	$\Omega$	
Oscillator grid leak . . . . .	$R_{gT+g3} =$	20	20	k $\Omega$	
Oscillator grid current . . . . .	$I_{gT+g3} =$	200	320	$\mu$ A	
Grid bias . . . . .	$V_{g1} =$	-1.0 -12 -1.8 -20 V			
Screen grid voltage . . . . .	$V_{g2+g4} =$	53	69	87	117 V
Anode current . . . . .	$I_a =$	1.0	—	2.2	— mA
Screen grid current . . . . .	$I_{g2+g4} =$	1.0	—	1.9	— mA
Conversion conductance . . . . .	$S_c =$	320	5.5	450	7 $\mu$ A/V
Internal resistance . . . . .	$R_i =$	1.4	>5	1.2	>5 M $\Omega$
Equivalent noise resistance . . . . .	$R_{eq} =$	115	—	145	— k $\Omega$

### Limiting values of the hexode section

Anode voltage, valve biased to cut-off . . . . .	$V_{a0}$	= max.	550 V
Anode voltage . . . . .	$V_a$	= max.	250 V
Anode dissipation . . . . .	$W_a$	= max.	0.8 W
Screen grid voltage, valve biased to cut-off . . . . .	$V_{(g2+g4)0}$	= max.	550 V
Screen grid voltage . . . . .	$V_{g2+g4}$	= max.	125 V
Screen grid dissipation . . . . .	$W_{g2+g4}$	= max.	0.3 W
Grid current starting point . . . . .	$V_{g1}(I_{g1} = +0.3\mu A)$	= max.	-1.3 V
Cathode current . . . . .	$I_k$	= max.	7 mA
External resistance between grid 1 and cathode . . . . .	$R_{g1}$	= max.	3 M $\Omega$

External resistance between grid 3 and cathode . . . . .	$R_{g3}$	= max.	3 M $\Omega$
External resistance between heater and cathode . . . . .	$R_{fk}$	= max.	20 k $\Omega$
Voltage between heater and cathode . . . . .	$V_{fk}$	= max.	150 V

**Limiting values of the triode section**

Anode voltage, valve biased to cut-off . . . . .	$V_{a_c}$	= max.	550 V
Anode voltage . . . . .	$V_a$	= max.	175 V
Anode dissipation . . . . .	$W_a$	= max.	0.75 W
Grid current starting point . . . . .	$V_g(I_g = +0.3 \mu\text{A})$	= max.	-1.3 V
Cathode current . . . . .	$I_k$	= max.	5.5 mA
External resistance between grid and cathode . . . . .	$R_g$	= max.	3 M $\Omega$
External resistance between heater and cathode . . . . .	$R_{fk}$	= max.	20 k $\Omega$
Voltage between heater and cathode . . . . .	$V_{fk}$	= max.	150 V

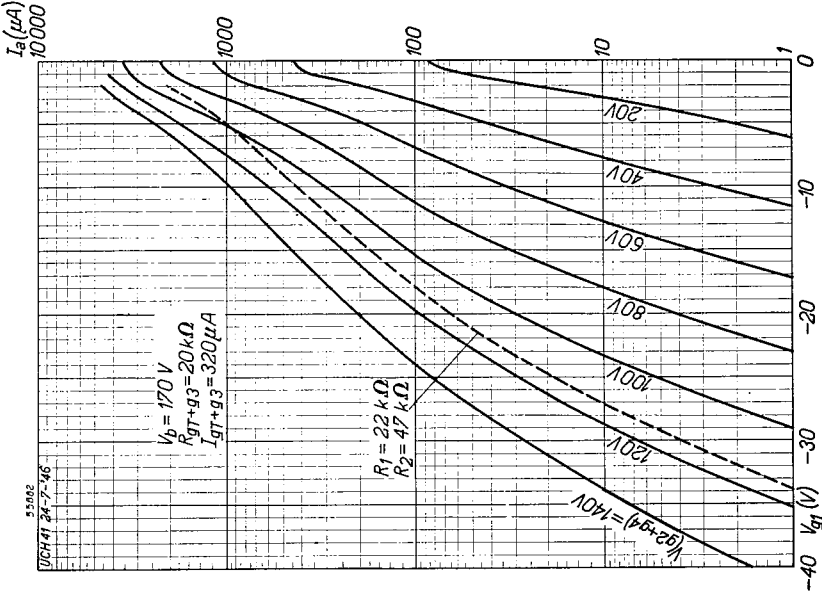


Fig. 7

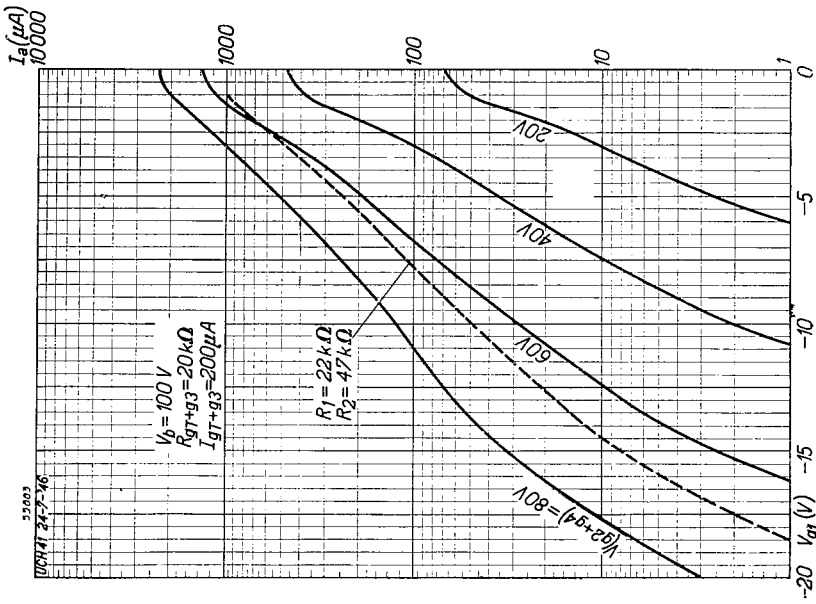


Fig. 6

Anode current ( $I_a$ ) of the UCH 41, measured on oscillating valve, as a function of the grid bias ( $V_{g1}$ ) with screen grid voltage ( $V_{g2+g3}$ ) as parameter. The dotted curves represent the anode current when the screen grid voltage is derived from a potentiometer ( $R_1, R_2$ , see Fig. 3). Fig. 6: supply voltage  $V_b = 100 \text{ V}$ ; Fig. 7:  $V_b = 170 \text{ V}$ .

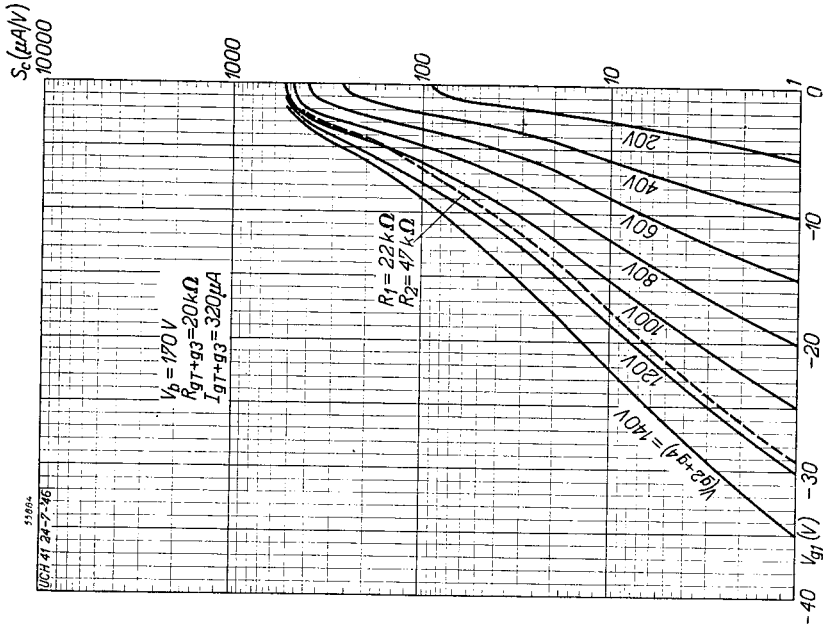


Fig. 9

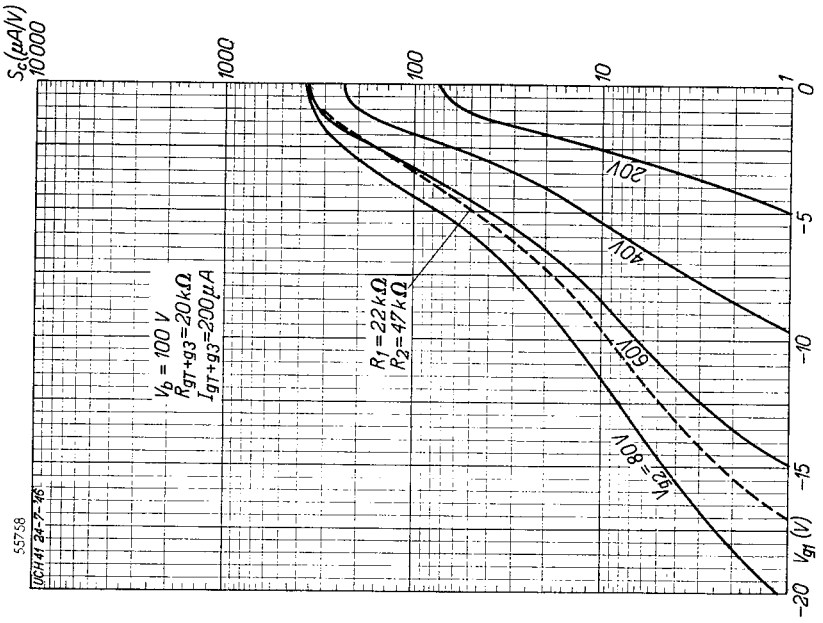


Fig. 8

Conversion conductance ( $S_c$ ) of the UCH 41, measured on oscillating valve, as a function of the grid bias ( $V_{g1}$ ), with screen grid voltage ( $V_{g2+g4}$ ) as parameter. The dotted curves represent the conversion conductance when the screen grids are fed by means of a potentiometer ( $R_1, R_2$ , see Fig. 3). Fig. 8 : supply voltage,  $V_b = 100 \text{ V}$ ; Fig. 9 :  $V_b = 170 \text{ V}$ .



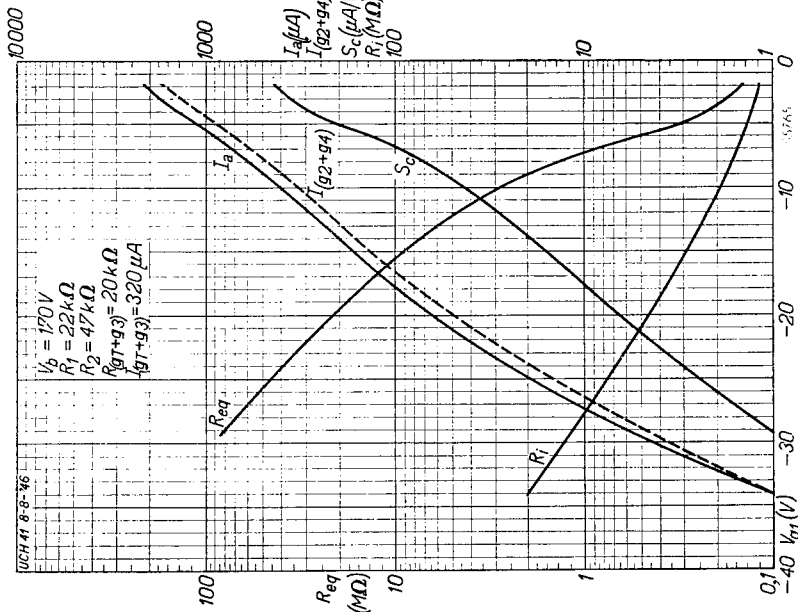


Fig. 11

Fig. 11:  $V_b = 170\text{ V}$ . Anode current ( $I_a$ ), screen grid current ( $I_{sg}$ ), conversion conductance ( $S_c$ ), internal resistance ( $R_i$ ) and equivalent noise resistance ( $R_{eq}$ ) of the UCH 41, as functions of the grid bias ( $V_{gr}$ ). Measurements taken from oscillating valve in circuit shown in Fig. 3.

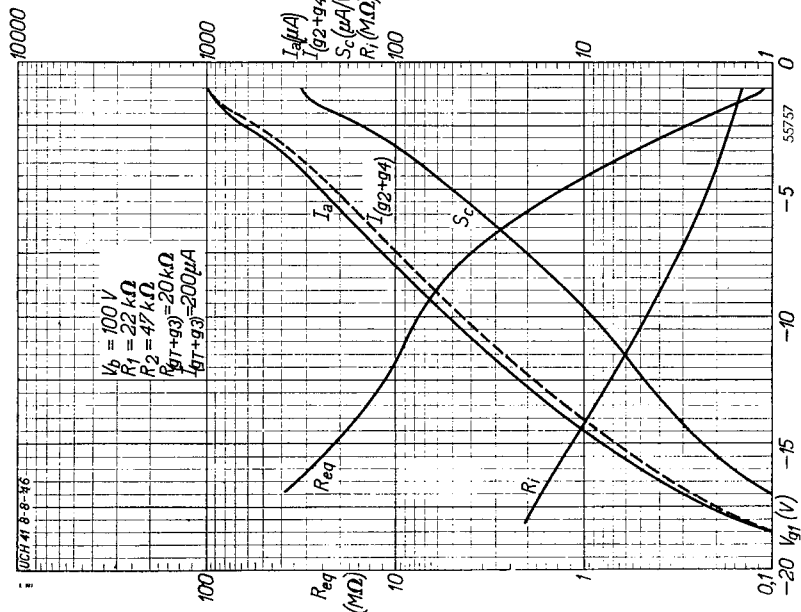


Fig. 10

Fig. 10:  $V_b = 100\text{ V}$ . Anode current ( $I_a$ ), screen grid current ( $I_{sg}$ ), conversion conductance ( $S_c$ ), internal resistance ( $R_i$ ) and equivalent noise resistance ( $R_{eq}$ ) of the UCH 41, as functions of the grid bias ( $V_{gr}$ ). Measurements taken from oscillating valve in circuit shown in Fig. 3.

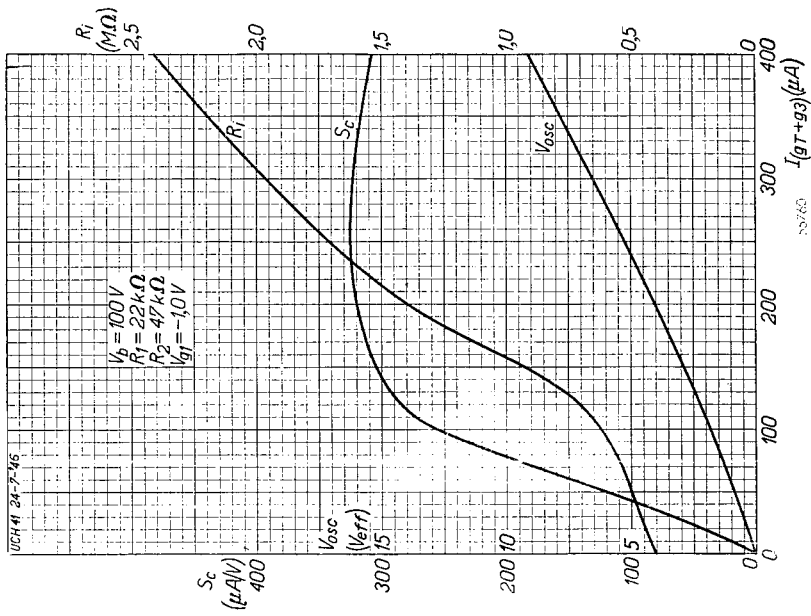


Fig. 12  
 Conversion conductance ( $S_c$ ), oscillator voltage ( $V_{osc}$ ) and internal resistance ( $R_i$ ) of the UCH 41, as functions of the oscillator grid current ( $I_{gr+g3}$ ). Relative to the circuit depicted in Fig. 3. Fig. 12 :  $V_b=100\text{ V}$  ;  $V_b=170\text{ V}$ .

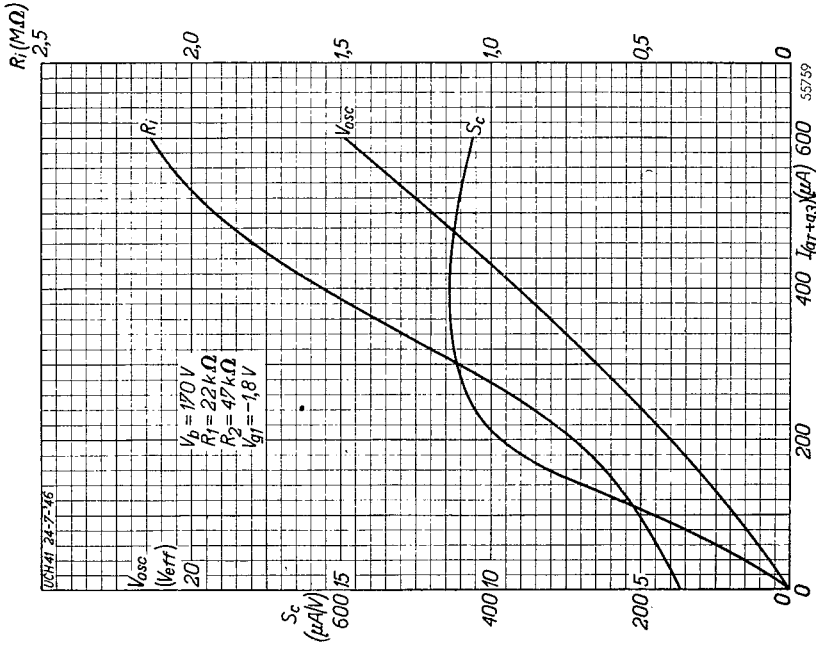


Fig. 13  
 Conversion conductance ( $S_c$ ), oscillator voltage ( $V_{osc}$ ) and internal resistance ( $R_i$ ) of the UCH 41, as functions of the oscillator grid current ( $I_{gr+g3}$ ). Relative to the circuit depicted in Fig. 3. Fig. 13 :  $V_b=100\text{ V}$  ;  $V_b=170\text{ V}$ .

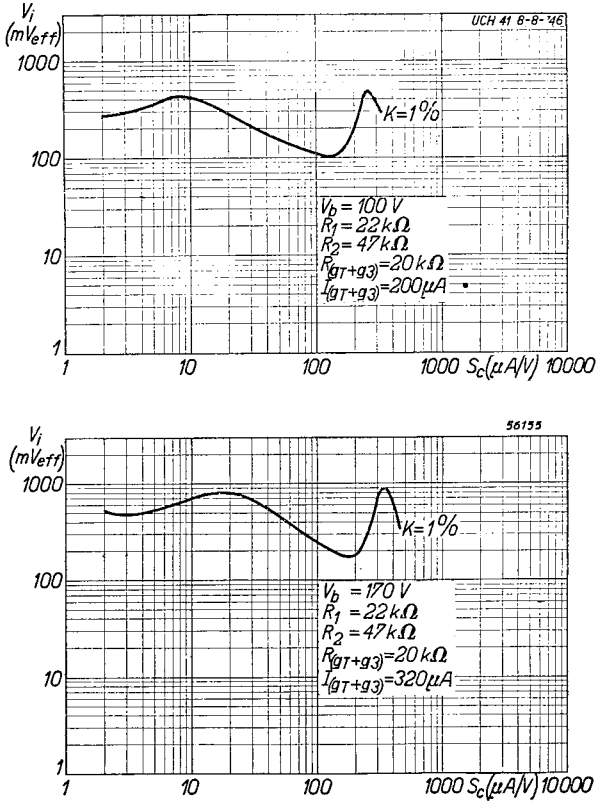


Fig. 14

The effective voltage ( $V_i$ ) of an interfering signal at the control grid of the UCH 41, producing 1% cross modulation, as a function of the conversion conductance ( $S_c$ ). Measurements taken in the circuit shown in Fig. 3. Upper figure:  $V_b=100 V$ ; lower figure:  $V_b=170 V$ .

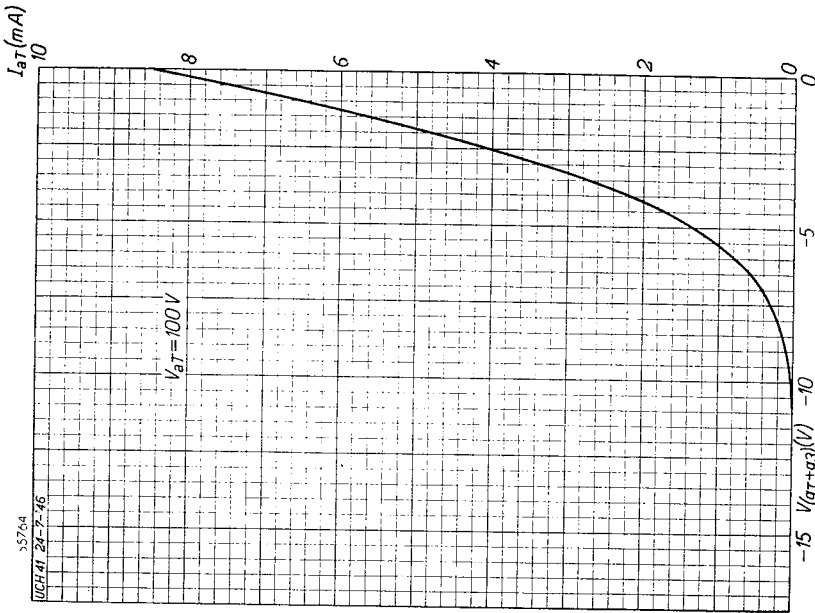


Fig. 15  
 $I_a/V_g$  characteristic of the triode system of the UCH 41.

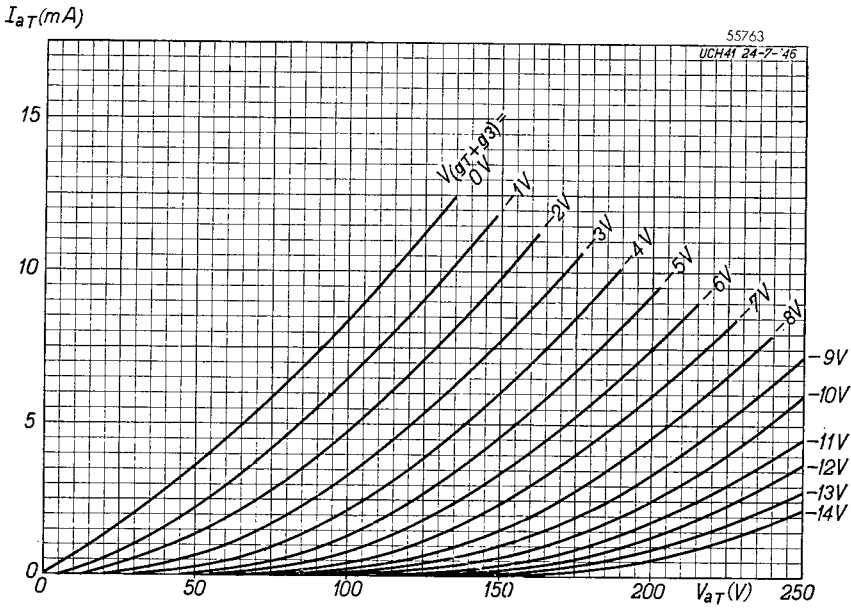


Fig. 16  
 $I_a/V_a$  characteristics of the triode system of the UCH 41.

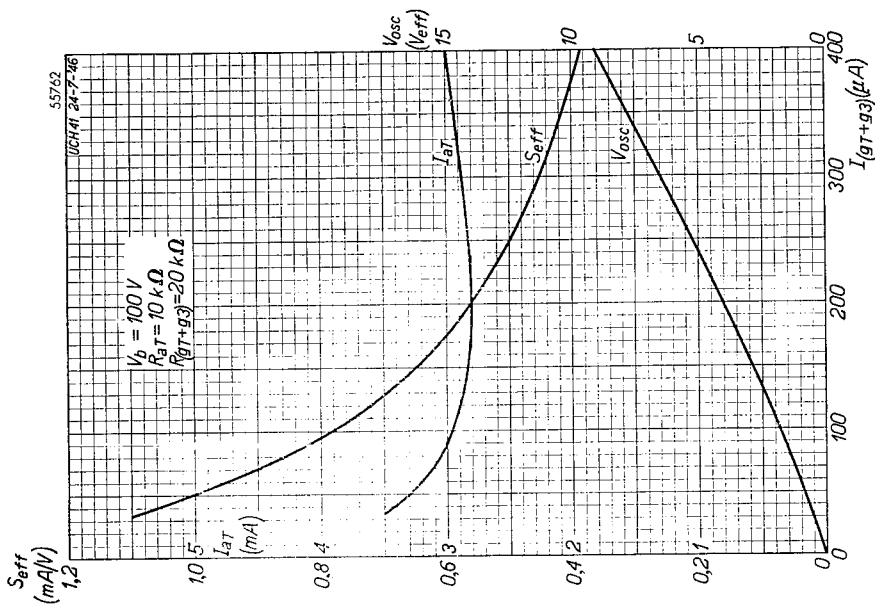


Fig. 17

Anode current ( $I_a$ ), oscillator voltage ( $V_{osc}$ ) and effective slope ( $S_{eff}$ ) of the triode system of the UCH 41, as functions of the oscillator grid current ( $I_{grT+g3}$ ). Fig. 17: supply voltage  $V_b = 100\text{ V}$ ; Fig. 18:  $V_b = 170\text{ V}$ .

Fig. 18

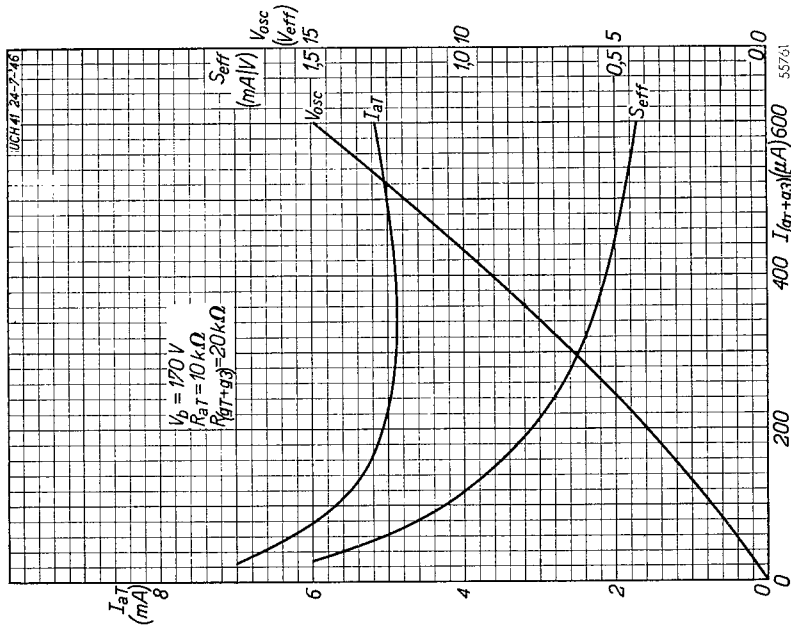


Fig. 18

Anode current ( $I_a$ ), oscillator voltage ( $V_{osc}$ ) and effective slope ( $S_{eff}$ ) of the triode system of the UCH 41, as functions of the oscillator grid current ( $I_{grT+g3}$ ). Fig. 17: supply voltage  $V_b = 100\text{ V}$ ; Fig. 18:  $V_b = 170\text{ V}$ .

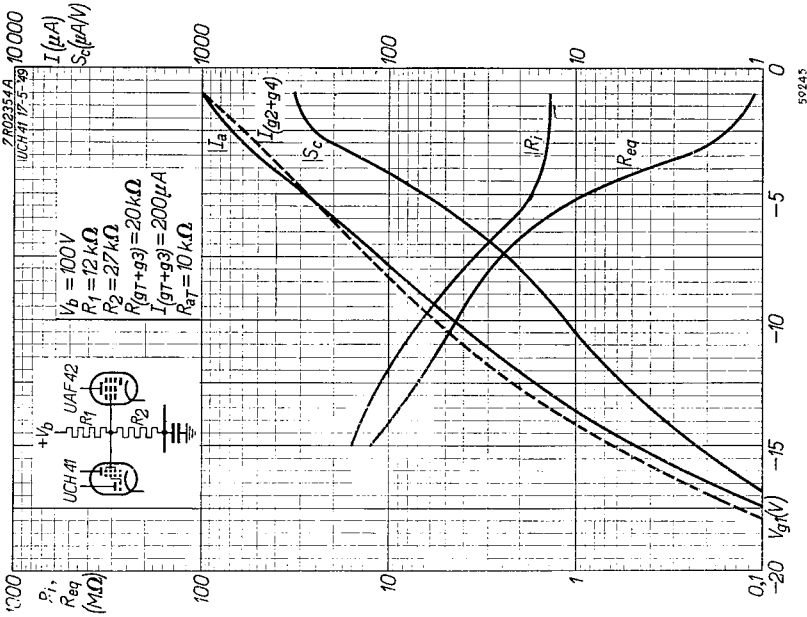


Fig. 19

As Fig. 10 and Fig. 11, but with the screen grids of the UCH 41, together with that of the UAF 42, fed by means of a common potentiometer. Measurements taken in the circuit shown in Fig. 5. Fig. 19: supply voltage  $V_b = 100 V$  ; Fig. 20 :  $V_b = 170 V$ .

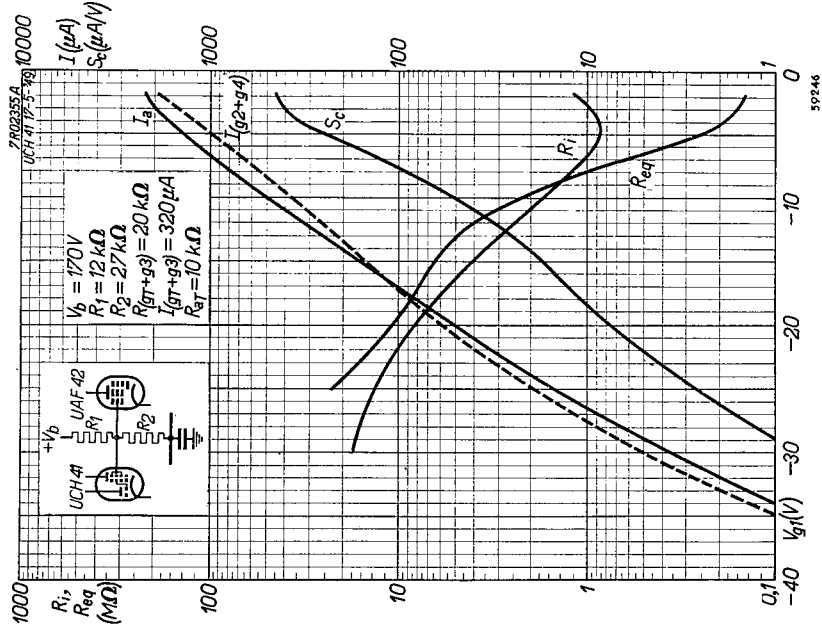


Fig. 20

As Fig. 10 and Fig. 11, but with the screen grids of the UCH 41, together with that of the UAF 42, fed by means of a common potentiometer. Measurements taken in the circuit shown in Fig. 5. Fig. 19: supply voltage  $V_b = 100 V$  ; Fig. 20 :  $V_b = 170 V$ .

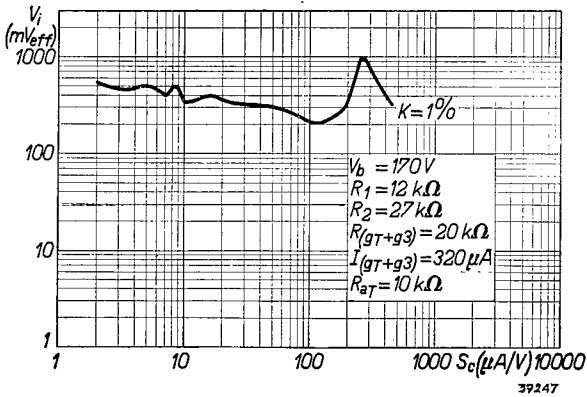
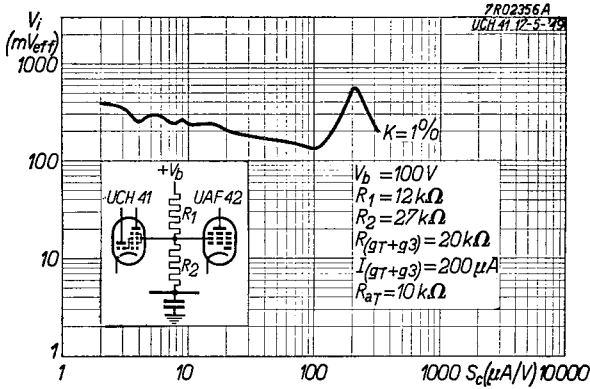


Fig. 21  
 As Fig. 14, but with screen grids of the UCH 41, together with that of the UAF 42, fed by means of a common potentiometer.